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Abstract: Incidental losses of dissolved reactive phosphorus (DRP) to a surface waterbody originate from direct losses during land application of fertilizer, or where a rainfall event occurs immediately thereafter. Another source is the soil. One way of immobilising DRP in runoff before discharge to a surface waterbody, is to amend soil within the edge of field area with a high phosphorus (P) sequestration material. One such amendment is iron ochre, a by-product of acid mine drainage. Batch experiments utilising two grassland soils at two depths (topsoil and sub-soil), six ochre amendment rates (0, 0.15, 1.5, 7.5, 15 and 30 g kg-1 mass per dry weight (dwt) of soil) and five P concentrations (0, 5, 10, 20 and 40 mg L-1) were carried out. A proportional equation, which incorporated P sources and losses, was developed and used to form a statistical model. Back calculation identified optimal rates of ochre amendment to soil to ameliorate a specific DRP concentration in runoff. Ochre amendment of soils (with no further P inputs) was effective at decreasing DRP concentrations to acceptable levels. A rate of 30 g ochre kg-1 soil was needed to decrease DRP concentrations to acceptable levels for P inputs of ≤ 10 mg L-1, which represents the vast majority of cases in grassland runoff experiments. However, although very quick and sustained metal release above environmental limits occurred, which makes it unfeasible for use as a soil amendment to control P release to a waterbody, the methodology developed within this paper may be used to test the effectiveness and feasibility of other amendments.

1 The Effectiveness and Feasibility of using Ochre as a Soil

2 Amendment to Sequester Dissolved Reactive Phosphorus in

3 **Runoff**

4

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13 Abstract

14 Incidental losses of dissolved reactive phosphorus (DRP) to a surface waterbody originate from direct losses during land application of fertilizer, or where a rainfall 15 16 event occurs immediately thereafter. Another source is the soil. One way of 17 immobilising DRP in runoff before discharge to a surface waterbody, is to amend soil 18 within the edge of field area with a high phosphorus (P) sequestration material. One 19 such amendment is iron ochre, a by-product of acid mine drainage. Batch experiments 20 utilising two grassland soils at two depths (topsoil and sub-soil), six ochre amendment rates (0, 0.15, 1.5, 7.5, 15 and 30 g kg⁻¹ mass per dry weight (dwt) of soil) and five P 21 concentrations (0, 5, 10, 20 and 40 mg L⁻¹) were carried out. A proportional equation, 22 23 which incorporated P sources and losses, was developed and used to form a statistical 24 model. Back calculation identified optimal rates of ochre amendment to soil to 25 ameliorate a specific DRP concentration in runoff. Ochre amendment of soils (with no further P inputs) was effective at decreasing DRP concentrations to acceptable levels. 26 A rate of 30 g ochre kg⁻¹ soil was needed to decrease DRP concentrations to 27 acceptable levels for P inputs of $\leq 10 \text{ mg L}^{-1}$, which represents the vast majority of 28 29 cases in grassland runoff experiments. However, although very quick and sustained 30 metal release above environmental limits occurred, which makes it unfeasible for use 31 as a soil amendment to control P release to a waterbody, the methodology developed 32 within this paper may be used to test the effectiveness and feasibility of other 33 amendments.

34

35 Keywords: phosphorus, adsorption, ochre, water quality

- 36
- 37

38 **1 Introduction**

39

40 Incidental losses of dissolved reactive phosphorus (DRP) in runoff on dairy farms 41 following a rainfall event originate from two sources: organic and inorganic fertilizer 42 inputs to grow grass and P from the soil (Preedy et al. 2001). One way of 43 immobilising this P before discharge to a surface waterbody, is to amend soil in a 44 riparian zone with a material that has a high P sequestration capacity. Iron-rich 45 materials have been used to sequester P from wastewater (Gallimore et al. 1999; Elliot 46 et al. 2002; Rhoton and Bigham, 2005; Johansson-Westholm, 2006; Brennan et al. 47 2011; Fenton et al. 2011). The capacity of ochre to sequester P from agricultural and 48 municipal wastewater has previously been investigated for ochre from coal mining 49 areas of the U.K. (Bozika, 2001; Heal et al. 2005; Dobbie et al. 2009), the U.S (Sibrell 50 et al. 2009) and metal mining areas of south east Ireland (Fenton et al. 2007). In 51 saturation experiments using low concentrations of inorganic P, Fenton et al. (2007) found that the maximum P retention capacity was approximately 19 g P kg⁻¹, for metal 52 53 mining ochre sourced from an abandoned copper sulphur mine in the Avoca-54 Avonmore catchment. In addition, kinetic experiments showed that P removal by 55 Avoca ochre to be very rapid. For example, the supernatant ortho-P (PO₄-P) 56 concentration decreased by 97% (Fenton et al. 2009a) within 5 minutes of shaking an 57 ochre/P-enriched mixture. However, the maximum P retention capacity for coal mining iron ochre is site-specific: 26 g P kg⁻¹ in Polkemmet, Central Scotland, and 58 30.5 g P kg⁻¹, in Minto, Central Scotland (Heal et al. 2004). A long-term field study 59 60 utilising coal mining ochre in pellet and granular forms was successful in reducing 61 total phosphorus (TP) concentrations without metal mobilisation (Dobbie et al. 2009). 62

63 Although the P adsorption capacity of Avoca ochre in the Fenton et al. (2009a) study 64 was comparable with ochre tested in the U.K., its characteristics were site-specific. 65 Fenton et al. (2009a) showed that Avoca ochre was fine-grained and had low particle density (2.3 g mL⁻¹), which facilitated entrainment and transportation in runoff during 66 67 flooding events. The study found that the high P adsorption capacity was due to high 68 iron (Fe) mineralogy. Iron minerals such as goethite, jarosite, hydronium jarosite, 69 lepidocrocite, and ferrihydrite, were found in the Avoca ochre, and P readily adsorbed 70 to their surfaces (Fenton et al. 2007). As the acid mine drainage (AMD) exited the 71 underground workings, oxidisation occurred, leading to ochre precipitation. This 72 resulted in higher concentrations of calcium (Ca), Cu, potassium (K), magnesium 73 (Mg), sodium (Na) and zinc (Zn) in the ochre than in the tributary water. Some 74 elements in the AMD ochre were as a result of background geology, while others 75 were directly related to the mining on site. Stereomicroscopy of this ochre identified 76 oolites and diatoms, which were indicative of an AMD environment (Fenton et al. 77 2009b).

78

79 Best management practices (BMPs) 'at source' (e.g. on the farmyard) aim to reduce 80 the amount of P lost in runoff and drainage waters. A common BMP is a riparian 81 buffer, or vegetative buffer strip, which limits P movement pathways from the field to 82 a waterbody (Sharpley et al. 2006). These vegetative buffer, or filter, strips are 83 effective in particulate phosphorus (PP) removal and have removal rates of between 84 45% (by concentration) (Schmitt et al. 1999) and 90% (by concentration) (Abu-Zreig 85 et al. 2003), but have limited removal capacity in relation to dissolved reactive 86 phosphorus (DRP) (Sharpley et al. 2006; Dorioz et al. 2006).

87

88	Application of P-immobilizing materials (alum, water treatment residuals (WTR), fly
89	ash, gypsum) to such vegetative buffer (or filter strips) through amendment of edge-
90	of-stream soils, is one possible means of reducing soluble P losses to aquatic systems
91	(Penn et al. 2007; Wagner et al. 2008; Brennan et al. 2011; Fenton et al. 2011). In
92	Ireland, soils receiving inorganic fertilizers as part of the Nitrates Directive (SI 610 of
93	2010) must maintain vegetative buffer zones at a minimum of 1.5 m in width from
94	river bank edge. For organic manures, this width is generally 5 m, but for narrow,
95	small parcels (< 1 ha) of land, it is 3 m. For steep slopes > 10%, it is 5 m, and for
96	Karst areas or water abstraction points, larger buffer distances of 250 m must be
97	maintained. In the current Agri-Environmental Options Scheme, a 1.5 m fenced buffer
98	must be established to prevent bovine access to the water course. Other agri-
99	environment schemes across Europe have similar stipulations (EC 2005).
100	
101	The present study examines P sequestration and metal losses from ochre amended
102	soils. The ochre was derived from AMD along a ditch running from the Deep Adit
103	site northeast of Whitebridge to the River Avoca (60 m downstream) (Fig 1).
104	Specifically, the objectives of this paper are:
105	1) to determine the optimal rate of ochre, or similar P sorbing amendments to soil,
106	to produce a given DRP concentration in runoff, to minimise losses to a surface
107	water body.
108	2) to determine if Avoca ochre, when mixed with soil, may be used as a safe soil
109	amendment to sequester P.
110	
111	2 Materials and Methods
112	

1	1	4
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115	Ochre from Whitebridge, Avoca, Co. Wicklow, south east Ireland (latitude 52° 48'N,
116	longitude 6° 12'W, mean precipitation 1200 mm and temperature 9.6 °C) was
117	collected, oven dried, sieved to < 2mm, and physically characterised in a previous
118	study (Fenton et al. 2009a).
119	
120	The P adsorption study was conducted using two permanent grassland soils taken
121	from Johnstown Castle Research Centre (latitude 52° 12' N, longitude 6° 30'W, mean
122	annual precipitation 1002 mm and temperature 9.6 °C). Each soil was sampled at two
123	depths:
124	• Soil A (classified as a humic cambisol after the World Reference Base
125	(WRB); Depth 1, top-soil (0 - 10 cm – standard Irish agronomic sampling
126	depth); Depth 2, sub-soil (11 - 30 cm)
127	• Soil B (WRB classification- gleyic cambisol); Depth 1, top-soil (0 - 10 cm);
128	Depth 2, sub-soil (11 - 30 cm)
129	
130	Incorporation of ochre at depth may be important where a perched watertable interacts
131	with buffer zones and contributes to runoff, or where DRP in runoff is leached to
132	groundwater.
133	
134	2.2 Physical characterisation of the soil and ochre
135	
136	Samples from both sites and depths were air dried, then sieved to $< 2mm$, wet sieved
137	into coarse sand (0.5 -2 mm), fine sand (0.053 - 0.5 mm), and silt/clay (<0.053 mm)

fractions, and then oven dried and weighed. Particle size distribution (PSD) of the silt
clay fraction was carried out using the pipette method (BSI 1989; BS 1796).

140

141 2.3 pH, lime requirement, C/N ratio and background nutrient and metal status of soil142 and ochre

143

144 Soil from both sites and depths, ochre samples, and ochre-amended soils from both 145 sites and depths used in batch experiments, were first analysed for pH in water using 146 an automated Gilson 215 liquid handler dip system (Middleton, Wisconsin, USA) 147 (n=4). The soil-to-distilled water ratio was 1:2, and samples were allowed to settle for 148 no more than 5 minutes before analysis. For quality control, a laboratory soil of 149 known pH and nutrient status was used. The control had the following characteristics 150 and no significant difference was found when analysed with the samples from the present study: pH - 5.89; Mg - 205 mg kg⁻¹; K - 72 mg kg⁻¹; and P - 5.3 mg kg⁻¹. 151 152 153 The lime requirement (LR) of all soils (i.e. the lime required to adjust soil to a pH of 154 6.3) was determined after Pratt and Blair (1963). In this procedure, 10 ml of soil per 155 volume was added to 20 ml of Shoemacher-McLean-Pratt (SMP) buffer (pH 7.5), 156 shaken for 30 min on a G10 gyratory shaker (New Brunswick Scientific, Edison, New 157 Jersey, USA), and poured through a No. 2 Whatman filter (0.2 µm) before analysis on 158 a flow-Gilson 215 liquid handler. Total organic carbon (TOC) and nitrogen (N) of the 159 soils was determined by placing 0.25 g of soil and standard samples in a porcelain 160 combustion boat on a CN2000 analyser (Leco Corporation, U.S.A).

161

162	In Ireland, the soil test phosphorus (STP) is classified using Morgan's extraction
163	solution. An index varying from 1 to 4 is applied, depending on the STP of a soil.
164	STP Index 1 represents a mineral soil with a P range of 0 to 3 mg L^{-1} , whereas a STP
165	Index 2 represents a P range of 3 to 5 mg L^{-1} . Index 3 represents a range of 3 to 8 mg
166	L^{-1} and Index 4 is >8 mg L^{-1} . Soil A (Depth 1) had a STP of 5.5 mg L^{-1} and Depth 2
167	had a STP of 2.6 mg L^{-1} . Soil B (Depth 1) had a STP of 2.8 mg L^{-1} and Depth 2 had a
168	STP of 2.7 mg L^{-1} (Table 1). This low STP minimised native P desorption during the
169	experiments. Optimum growing conditions for grassland is STP Index 3 with a soil P
170	range of 3 to 8 mg L^{-1} for mineral soils. Soil test phosphorus was measured as
171	Morgan's phosphorus (P_m ; mg L ⁻¹) and converted to Mehlich 3 phosphorus (M3P; mg
172	kg ⁻¹) for indicative purposes, using the following equation (Tunney et al. 1998):
173	

174
$$M 3P = 8.52 * P_m^{0.85}$$
 [1]

Oven dried soil samples, with a grain size < 2mm (6 replicates for each soil type), were analysed for STP, Mg and K as follows: 3 mL of soil by volume was added to 15 mL of Morgan's extracting solution in a round-bottomed flask and shaken on a G10 gyratory shaker for 30 min. The suspension was then filtered through a No. 2 Whatman filter into disposable test tubes and analysed colorimetrically using the chemical reaction between P and ammonium molybdate.

182

183 To investigate metal mobilisation and the suitability of metal mining ochre to

184 sequester P from runoff, the supernatant water from all batch experiments was

185 analysed for trace metals (cadmium (Cd), chromium (Cr), Cu, iron (Fe), manganese

- 186 (Mn), nickel (Ni), lead (Pb) and Zn) using an ICP-MS. Metal release from ochre-
- 187 amended soil over time was carried out in a kinetic test at 1, 5, 10, 15, 30, 60 min.188

189 2.4 Batch experiment with soil and ochre amendment

190

191To achieve a homogenous < 2 mm mix, the soils were saturated with distilled water,</th>192manually mixed into a slurry, and left to air dry for 60 d. After this time, ochre was193mixed to soil aliquots in the following proportions: 0 (the study control), 0.15, 1.5,1947.5, 15 and 30 g ochre kg⁻¹ mass per dry weight (dwt) of soil. Such amendment rates195were also used for ferrihydrite (Fe₅HO₈·4H₂O) amendments to soils for P

196 sequestration (Rhoton and Bigham 2005).

197

198 The ochre amendment was applied during continuous mixing of the soil with a spray 199 of distilled water to allow greater incorporation of the ochre into the soil. Next, the 200 soil and ochre mix was air dried, and the bulk dry samples were crushed, rolled and 201 sieved to < 2 mm. All batch experiment protocols were carried out after Cucarella and 202 Renman (2009). For each soil and depth, in each 100-ml- capacity container, 2.5 g of 203 oven dried-ochre-and-soil mixture (mixed in the ratios described above) and air dried 204 soil-only was overlain with 50 ml of synthetic P solution (potassium phosphate (KH_2PO_4) with concentrations of 0, 5, 10, 20, or 40 mg P L⁻¹ (n=2). Although end-205 206 over-end shakers do not simulate overland flow, for consistency with other studies, 207 the samples were sealed and then mixed in an end-over-end shaker for 24 hr, after 208 which the samples were vortexed for 2 min, centrifuged at 100 rpm for 10 min, filtered and analysed for DRP in a nutrient analyser (Konelab, Ontario, USA). 209 210

A proportional equation, which incorporated P sources (P inputs) and losses (DRP
losses in runoff and STP), was developed. Back calculation identified optimal rates of

- 215 ochre amendment to soil to ameliorate a particular DRP concentration in runoff.

216

217 In the batch experiment, ochre with negligible background P content was added to a

218 soil of known STP. This content was based on historic records of inorganic and

219 organic fertilizer application. P_{Lost} (%) was calculated as:

220

221
$$P_{\text{Lost}}(\%) = \frac{P_{\text{Runoff}}}{P_{\text{Input}} + \text{STP}} *100$$
 [2]

222

The proportion of P not adsorbed by the amendment after P equilibrium (P_{Lost}; %) 223 depends on the P in runoff (P_{Runoff} ; mg L⁻¹) that has not been adsorbed to the ochre; 224 the Morgan's STP of the soil before any ochre amendment (STP; mgL^{-1}); and the P 225 added in the batch experiments or as a fertilizer (P_{Input} ; mg L⁻¹). A high P_{Lost} (%) 226 227 signifies a greater amount of P in solution available to be lost to a waterbody and a low P_{Lost} signifies more P has been adsorbed by the ochre. Statistical analysis was 228 229 conducted in SAS v 9.1, using a generalised linear mixed model (GLMM) with a logit 230 link and a normal distribution:

231

$$232 \qquad x\beta = \ln\left(\frac{P_{\text{Lost}}}{1 - P_{\text{Lost}}}\right)$$
[3]

234	where $1-P_{Lost}$ is P adsorbed onto ochre. The effects of ochre additions, P_{Input} , soil type,
235	and soil depth (topsoil or subsoil), and their interactions were tested in the model
236	using Type III tests of fixed effects. The background pH of the soils before
237	amendments was variable. To compare results, pH needed to be accounted for in the
238	statistical analysis. The soil variation was accounted for by including pH, determined
239	in a SMP buffer, as a random effect.
240	
241	After initial analysis was complete, back-calculation within the model made it
242	possible to predict P_{Runoff} . This then allowed calculation of the amount of ochre
243	amendment needed per kg of soil to reduce P_{Runoff} to acceptable levels.
244	
245	3. Results & Discussion
246	
247	3.1 Physical characterisation of soil
248	
249	The PSD of both soils are presented in Table 1. Soil A (Depth 1) contained a higher
250	sand fraction and lower silt and clay fractions than Depth 2. There was a slight
251	textural change with depth, but it remained within the sandy-loam textural class. Soil
252	B (Depth 1 and 2) had similar coarse and fine sand fractions, but differed with respect
253	to their silt and clay fractions. Both soil depths also had a sandy-loam textural class.
254	Both soils were well-drained in the field and it was easy to amend the soils with
255	ochre.
256	
257	Physical characterisation of the ochre used in this study was carried out by Fenton et
258	al. (2009a). The ochre was fine-grained with the following constituency: coarse sand,

259 21.6% by mass; fine sand, 19.5% by mass; silt, 22.3% by mass; and clay, 30.9% by
260 mass.

261

262 3.2 STP, pH and C/N ratio

263

264 The study sites had similar topography and low to very low STP (Table 1). Such STP 265 concentrations are deemed environmentally sound and thereby minimised native P 266 desorption during the experiments. The average pH of all soils and soil depths was 267 6.5±0.6, which is the optimal pH for grass growth. With little ochre amendment, pH 268 remained at, or above, this optimal pH. At higher amendment rates (7.5 - 15 g ochre)kg⁻¹ mass per dwt of soil), Depth 1-soils become acidic and would need lime 269 270 correction to maintain grass growth. Leonard et al. (2006) found that the mean C/N 271 ratio was 12.0±1.8, compared with 8.8 and 12.5 for Soils A and B, respectively (Table 272 1). Such results match the soil P status of the soils used in the current study i.e., low 273 fertilizer inputs and risk of P loss to surface water. 274 3.3 PLost and PRunoff 275

276

All factors tested (Soil, ochre, P, ochre*P, ochre*Soil, Soil*P, and ochre*Soil*P) had a significant influence on P_{Lost} , so no terms were removed from the predictive statistical model (Table 2). For Soil (A, B) Depth (1, 2), the regressions of P_{Lost} against ochre amendment are displayed in Figures 2 and 3. The slopes and intercepts of the predicted lines using the P_{Lost} equation differed depending on the amount of P_{Input} . Statistically, differences in background soil pH before any ochre amendment explains variation in P_{Lost} between soils. Predicted lines occurred at an average pH for

that soil and ochre interaction. Actual and predicted results showed good agreement,

which allowed prediction of DRP in solution for given P inputs and ochre amounts onthese soils.

287

The P index of the soils ranged from 1 to 3. Soils in Index 1 and 2 are P deficient, 288 289 while in Index 3 are at target index, with a low risk of loss to water. This indicates P 290 concentrations from these soils in runoff will not affect maximum admissible concentrations i.e. 0.035 mg DRP L^{-1} due to dilution in the surface water body. 291 Phosphorus losses from Index 2-3 soils can still be quite high; for example, Kurz et al. 292 (2005) found DRP in runoff ranged from <0.005 to 0.19 mg L⁻¹ before fertilization 293 and 1.38 mg L^{-1} after fertilization on grassland soils. For soils with no ochre or P 294 amendment, the P_{Runoff} concentrations were within this range (Table 3). Any P 295 addition increased P_{Runoff} , but ochre amendment (≥ 1.5 g ochre kg⁻¹ soil) was 296 297 successful in decreasing DRP losses. There was no significant difference between 0 and 0.15 g ochre kg⁻¹ soil results. Ochre amendment to soil without any P inputs 298 substantially decreased DRP losses. A rate of 30 g ochre kg⁻¹ soil was needed to 299 decrease DRP concentrations to acceptable levels for P inputs of $< 10 \text{ mg L}^{-1}$, which 300 301 represents the vast majority of cases in grassland runoff experiments. 302 303 3.4 Metal mobilisation during batch experiments

304

305 The ochre had the following metal content: Al, 4.8 ± 0.0 g kg⁻¹; Cu 0.3 ± 0.0 g kg⁻¹,

306 Fe, 246 ± 0.0 g kg⁻¹; Mg, 0.5 ± 0.0 g kg⁻¹; arsenic (As), 162 ± 18.3 mg kg⁻¹; Cd, 3.2 ± 0.3

307 mg kg⁻¹; Cr, 3.1 ± 1.8 mg kg⁻¹; Pb, 2087 ± 75.3 mg kg⁻¹; nickel (Ni), 1.7 ± 0.9 mg kg⁻¹;

308 and Zn, 250 ± 19.8 mg kg⁻¹. In the present study, the ratio of ochre to solution was

309 1:20. Average mobilisation of metals into solution after 24 h for distilled water amended with ochre was: Cu, 14,044 \pm 290 µg L⁻¹; Fe, 1892 \pm 109 µg L⁻¹; K, 123 \pm 1.6 310 mg L^{-1} ; Mg, 1.78±0.2 mg L^{-1} ; Mn, 323±30.4 µg L^{-1} ; Na, 2.9±0.2 mg L^{-1} ; and Zn, 311 $18034\pm795 \ \mu g \ L^{-1}$. The pH of ochre in distilled water was 3, thereby allowing for 312 313 greater metal release. The soil and ochre combinations reduced much of the metal 314 mobilisation, but not enough in some cases to prevent recommended limits (Table 4a 315 and 4b). The control soils without ochre amendment had, in some cases, metal 316 concentrations above allowable limits. Soil A had high Cd, Cr, Fe, Ni and Pb 317 concentrations and Soil B had high Cd, Pb and Zn concentrations. 318 319 Kinetic tests indicated that most of the metal mobilization occurred within 1 min of 320 mixing P solutions with the ochre (Table 5). For all metals, high concentrations were released in the first minute, decreased, and rose again after 1 hr. For P adsorption to 321 322 ochre, the opposite occurred, which involved rapid ligand exchange with surface

323 hydroxide groups at reactive sites and the formation of binuclear bridging complex324 between a phosphate group and two Fe surface atoms, followed by a weaker ligand

325 exchange.

326

There has been some documentation of hazardous release of metals from coal mining ochre in 5 out of 49 mine-water treatment facilities in the U.K. (Hancock 2005). The ochre used in this study released toxic concentrations of metals in runoff. Inductively coupled plasma mass spectrometry and bulk energy dispersive spectroscopy showed potentially toxic concentrations of Fe, Zn, Pb, As and Cu (Fenton et al. 2009b). Remobilisation of heavy metals might occur due to any reduction of iron oxides in the soil and ochre, for example, by rising groundwater depths in a perched watertable

334 scenario e.g. glaciated tills or by incorporation into the buffer. International studies by 335 Winner et al (1980), Clements et al (1992) and Beltman et al (1999), have all shown 336 that discharge from AMD has negative effects on aquatic communities. These effects 337 include a reduction in species diversity and abundance, and a change in the 338 community structure from sensitive species such as Stonefly Larva to more tolerant 339 groups such as Tubificid worms. A study by Curran (2001) on the Avoca catchment, 340 found that there was a major decrease in aquatic invertebrate diversity and abundance 341 downstream from the Deep Adit discharge site (Figure 1). It was concluded that the 342 inflow adit ditch stream was uninhabitable for macro fauna because of its elevated 343 conductivity, acidic pH and high levels of metals and sulphates. Although these 344 concentrations will, to some extent, also be diluted by the main surface waterbody, 345 any release of toxic metal makes Avoca ochre unsuitable for use in buffer strips. 346

However, the methodology developed within this paper may be used to test theeffectiveness and feasibility of other amendments.

349

350 4 Conclusions

351 The findings of this grassland study are:

1. A proportional equation, which incorporated P sources and losses, was developed.

353 Back calculation identified optimal rates of ochre amendment to soil to ameliorate a

354 particular DRP concentration in runoff. A rate of 30 g ochre kg⁻¹ soil was needed to

- decrease DRP concentrations to acceptable levels for P inputs of $\leq 10 \text{ mg L}^{-1}$.
- 2. Very quick and sustained metal release from the ochre tested during P sequestration
- 357 makes it unsuitable for use as a soil amendment to control P release to a waterbody.
- 358 However, the methodology developed in this study allows the optimal rate of addition

359	of any P	sorbing	amendment,	when n	nixed v	with soil,	to reduce	the DRP	below a

360 certain threshold value, to be determined.

361

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- 364

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504 **Captions for Figures**

505 Fig 1 Schematic of Avoca Avonmore catchment and sampling location.

506	Fig 2 P_{Lost} (%) results and model predictions for both soils, soil depths for all ochre
507	amendments, and P concentrations (A-D). A high P_{Lost} (%) signifies a greater amount
508	of P in solution available to be lost to a waterbody and a low P_{Lost} (%) signifies more
509	P has been adsorbed by the ochre
510	
511	Fig 3 P_{Runoff} results and predictions for both soils, soil depths for all ochre
512	amendments, and P concentrations (A-D).
513	
514	
515	

Table 1 Soil particle size distribution and organic fraction analysis for Soil A and B, Depth 1 and 2.

 Soil (Depth)	Soil P Index	Coarse Sand	Fine Sand	Silt	Clay	С	Ν	C/N	Pm*	M3P**	Mg	К
			%			mg	kg ⁻¹			mg	kg ⁻¹	
Soil A (Depth 1)	3 (3.0-8.0 P_m -mg L ⁻¹)	43	25	30	2	2.1	0.2	8.8	5.5	36.2	206.2	102.8
Soil B (Depth 1)	1 (0.0-3.0 P_m -mg L ⁻¹)	26	14	45	15	0.2	-	-	2.6	19.1	202.7	122.1
Soil A (Depth 2)	1 (0.0-3.0 P_m -mg L ⁻¹)	40	30	17	13	1.5	1.2	12.5	2.8	20.4	256.9	199.8
Soil B (Depth 2)	1 (0.0-3.0 P_m -mg L ⁻¹)	48	28	6	18	0.7	-	-	2.7	19.8	212.1	132.0

517 *P_m- Morgan's P, **M3P - Mehlich 3 P

	Num - DF	Den - DF	F value	Pr > F
Soil	3	207	46.89	<.0001
Ochre	1	207	166.56	<.0001
Р	3	207	474.90	<.0001
Ochre*P	3	207	25.36	<.0001
Ochre*Soil	3	207	17.47	<.0001
Soil*P	9	207	7.36	<.0001
Ochre*Soil*P	9	207	3.44	0.0006

Table 2 Type 3 Tests of Fixed Effects

Table 3 Predicted P_{Lost} (%) and P_{Runoff} (mg L⁻¹) with different P and ochre

537 amendments.

Ochre amendment	P amendment									
g ochre kg ⁻¹ soil						mg P I	1			
	0	5	10	20	40	0	5	10	20	40
	P_{Lost} (%)						P	_{Runoff} (mg	$g L^{-1}$)	
0	3	15	39	50	62	0.109	2.5	5.2	11.7	26.9
0.15	3.2	16	38	56	75	0.113	2.6	5.1	13.1	32.3
1.5	2.3	12	33	51	70	0.076	2.1	4.5	12.0	30.5
7.5	0.9	3	22	32	56	0.027	1.5	3.0	7.5	24.5
15	0.6	2	10	23	46	0.018	0.8	1.4	5.5	19.8
30	0	0	3	11	36	<dl< td=""><td><dl< td=""><td>0.301</td><td>2.3</td><td>14.5</td></dl<></td></dl<>	<dl< td=""><td>0.301</td><td>2.3</td><td>14.5</td></dl<>	0.301	2.3	14.5

A high P_{Lost} (%) signifies a greater amount of P in solution available to be lost to a waterbody and a low P_{Lost} (%) signifies more P has been adsorbed by the ochre. Average P_{Runoff} after equilibrium with different P and ochre amendments. Both soils and soil depths included and all samples used (n=8). DL = detection limit

Table 4 a. Average mobilisation of metals (n=2) ± (standard deviation) into solution after 24 h. Soil A (Depth 1), all P concentrations and ochre

543 amendments

Ochre	Р	pН	Ca	±**	Cd	±	Cr	\pm	Cu	±	Fe	±	Κ	<u>+</u>	Mg	±	Mn	±	Na	±	Ni	±	Pb	±	Zn	±
g kg ⁻¹	mg L ⁻¹		mg L^{-1} µg L^{-1}																							
0	0	7.3	4.3	0.2	0.0	0.1	3.3	1.4	47.9	2.7	1500.1	478.0	4.1	0.3	1.5	0.1	2447.2	396.9	1.3	0.1	8.5	1.8	23.5	3.8	13.7	1.5
0	10	7.3	4.4	0.2	0.0	0.0	1.3	1.2	52.5	3.7	1055.4	703.2	10.5	0.2	1.5	0.1	2749.5	157.9	1.3	0.0	11.4	0.9	23.6	8.0	12.6	2.8
0	20	7.3	4.9	0.3	0.0	0.0	0.1	0.3	52.2	6.1	739.9	439.1	18.4	0.2	1.6	0.1	2972.2	209.9	1.3	0.1	10.1	2.2	25.8	5.6	12.6	4.7
0	40	7.3	5.2	0.5	0.0	0.0	1.7	3.3	46.5	15.2	486.5	508.9	36.4	1.1	1.6	0.2	2992.2	392.8	1.3	0.0	11.3	4.3	25.7	4.1	11.0	3.2
0.15	0	6.2	4.7	0.2	0.0	0.0	1.7	1.6	163.8	97.5	1495.0	1173.6	4.2	0.3	1.6	0.3	2900.0	458.0	1.3	0.0	10.1	1.5	36.6	7.9	17.6	4.1
0.15	10	6.2	4.6	0.2	0.0	0.0	0.0	0.2	79.7	3.4	594.9	465.8	10.8	0.0	1.5	0.0	2901.2	237.9	1.3	0.1	9.3	3.1	26.9	14.4	16.8	1.3
0.15	20	6.2	4.9	0.2	0.0	0.0	0.8	1.4	74.1	6.2	307.6	102.9	19.6	0.5	1.5	0.1	3126.8	200.7	1.3	0.1	6.4	4.0	32.9	10.8	13.3	1.2
0.15	40	6.2	6.0	0.4	0.0	0.0	0.5	0.1	81.8	12.6	405.6	101.9	37.1	0.5	1.9	0.1	3736.2	219.5	1.4	0.0	8.8	0.8	31.4	14.3	13.7	1.5
1.5	0	6.1	4.7	1.5	2.0	3.5	6.9	6.2	66.0	22.5	1966.2	2859.0	4.3	1.2	1.8	0.7	2828.9	898.9	1.3	0.4	15.1	8.6	18.3	18.1	21.1	13.2
1.5	20	6.1	5.9	0.5	1.0	1.4	7.1	4.6	85.7	9.4	1150.7	1497.5	11.7	0.6	1.9	0.3	3536.4	277.5	1.5	0.2	7.5	3.6	1.5	2.7	21.0	6.1
1.5	10	6.1	6.2	0.6	0.0	0.0	10.4	3.0	82.7	14.1	3010.4	1001.0	20.1	1.5	2.2	0.8	3770.1	394.6	1.4	0.1	12.5	7.2	5.1	5.0	24.7	15.7
1.5	40	6.1	6.7	0.7	0.0	0.0	4.8	1.4	71.1	12.5	277.5	19.0	37.7	1.5	2.0	0.2	3777.4	430.5	1.5	0.1	5.4	1.7	0.0	0.0	15.3	1.9
7.5	0	5.9	11.8	2.5	0.0	0.2	4.6	1.6	61.4	6.9	340.1	85.7	5.2	0.7	3.2	0.7	6713.2	1360.7	1.4	0.3	11.1	5.0	3.7	6.4	24.2	5.2
7.5	10	5.9	11.6	0.8	0.0	0.2	4.2	2.4	63.5	4.9	368.4	261.1	13.2	0.3	3.1	0.3	6545.3	463.8	1.4	0.1	8.8	5.7	0.0	0.0	27.6	1.0
7.5	20	5.9	11.6	0.6	0.1	0.2	9.1	6.8	76.3	14.6	2050.7	2989.2	22.2	1.1	3.3	0.5	6409.3	105.3	1.4	0.1	13.5	4.0	2.4	2.4	32.1	8.6
7.5	40	5.9	11.2	0.7	0.0	0.1	7.7	5.4	76.4	12.4	2301.0	3175.7	40.8	0.5	3.2	0.5	6201.6	399.6	1.3	0.1	14.9	5.7	4.8	8.3	31.7	9.8
15	0	5.7	17.0	1.1	0.0	0.0	3.6	1.3	76.5	13.2	739.2	356.0	5.8	0.1	4.2	0.2	10366.7	701.8	1.5	0.0	7.4	2.9	0.4	0.6	69.1	13.3
15	10	5.7	15.7	0.2	-0.1	0.1	6.0	1.8	97.9	4.8	655.5	284.0	13.6	1.2	3.9	0.0	9280.6	172.3	1.4	0.1	13.0	8.7	6.0	8.5	66.0	6.8
15	20	5.7	16.1	1.3	4.5	3.4	8.4	3.6	85.3	11.2	400.2	44.8	23.5	0.4	4.0	0.3	9604.4	726.7	1.5	0.2	13.0	5.6	11.9	10.5	72.8	5.2
15	40	5.7	16.0	0.5	0.7	0.3	5.2	5.5	95.0	41.2	1507.3	2105.7	50.8	6.7	4.0	0.5	9546.0	391.8	1.4	0.2	13.2	0.9	4.6	5.0	76.2	8.7
Limit*					0.2		0.6		5												20		7.2		40	

** standard deviation standards for surface waters (other than inland surface waters) (Council of the European Union, 2009) **± standard deviation

546 **Table 4 b.** Metal concentrations in solution after batch experiments (n=2) ± (standard deviation) with Soil B (Depth 1), all P concentrations and

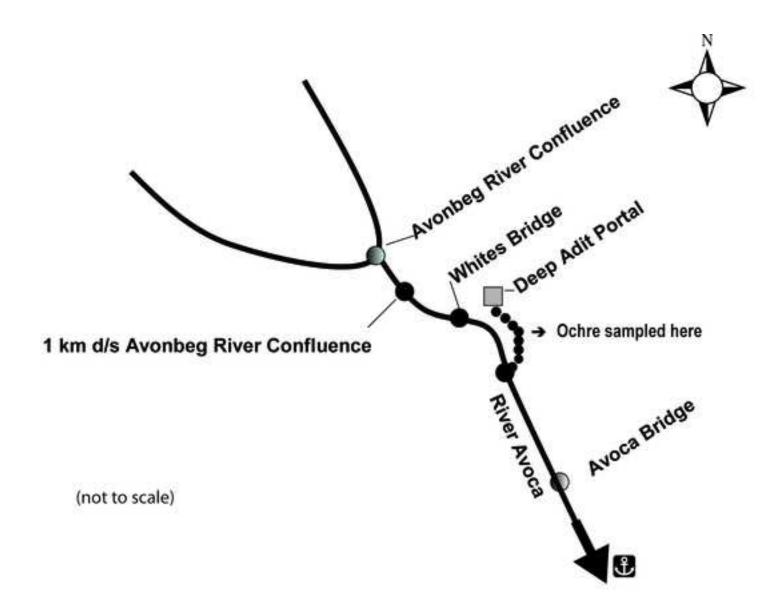
547 ochre amendments

Ochre	Р	pН	Ca	±**	Cd	±	Cr	±	Cu	±	Fe	±	K	±	Mg	±	Mn	±	Na	±	Ni	±	Pb	±	Zn	±
g kg ⁻¹	mg L ⁻¹		mg	L^{-1}											μg I	-1 _										
0	0	7.0	3.9	0.8	0.3	0.4	6.3	1.8	54.2	9.0	1518.7	707.6	3.4	0.5	1.8	0.4	573.3	181.9	1.4	0.0	4.0	1.1	12.0	6.9	28.8	8.9
0	10	7.0	2.2	0.6	0.1	0.1	5.7	1.0	58.2	5.6	965.0	90.7	9.7	0.4	1.5	0.2	527.6	81.4	1.4	0.2	2.4	1.6	0.0	0.2	32.5	4.9
0	20	7.0	2.8	0.2	0.0	0.2	7.5	1.0	61.4	2.8	1247.9	234.2	18.2	0.2	1.8	0.1	626.8	36.6	1.5	0.1	10.5	3.4	1.3	2.3	39.8	2.8
0	40	7.0	3.1	0.3	0.0	0.1	8.0	1.2	64.1	2.7	1201.7	245.1	41.3	1.1	1.8	0.0	621.8	48.0	1.7	0.3	7.4	2.2	2.6	3.9	39.5	4.3
0.15	0	5.9	3.6	0.7	0.4	0.7	4.9	1.8	37.6	7.5	1391.7	329.3	3.6	0.3	2.2	0.3	749.9	116.1	1.8	0.3	10.7	7.0	8.4	3.9	31.7	5.9
0.15	10	5.9	3.2	0.5	0.2	0.3	6.4	1.6	38.4	2.3	1352.8	147.1	11.1	0.4	2.0	0.1	722.0	74.9	1.7	0.1	8.6	1.9	9.1	15.8	35.1	1.7
0.15	20	5.9	3.7	1.1	0.0	0.1	14.2	2.5	52.5	10.5	2995.6	1450.3	20.6	0.6	2.5	0.5	797.9	194.4	1.9	0.2	12.3	6.5	13.0	9.9	46.4	12.7
0.15	40	5.9	4.5	0.6	3.5	6.0	9.6	4.2	53.8	15.4	1412.1	103.9	43.0	3.4	2.4	0.0	748.6	134.3	1.9	0.1	16.3	4.7	16.3	16.4	45.9	8.4
1.5	0	6.0	5.2	1.4	0.7	1.1	8.8	4.9	47.8	17.4	2098.5	1570.9	3.6	0.4	2.2	0.6	681.9	205.5	1.6	0.0	11.7	2.8	8.9	11.0	36.9	8.6
1.5	10	6.0	4.4	0.1	0.0	0.2	5.9	1.2	47.9	4.3	1481.6	105.7	9.9	0.1	1.7	0.0	596.1	12.0	1.6	0.1	9.9	4.1	17.4	16.6	39.1	2.8
1.5	20	6.0	4.5	0.2	0.0	0.2	3.7	0.4	53.5	2.5	1276.9	486.7	17.6	0.4	1.7	0.1	595.3	26.2	1.5	0.0	10.3	4.1	11.8	14.8	41.2	3.3
1.5	40	6.0	5.1	0.8	0.1	0.1	2.8	2.3	43.1	10.7	1017.3	269.9	39.0	1.9	1.9	0.2	632.7	92.6	1.8	0.3	4.8	5.2	7.9	6.1	39.5	5.4
7.5	0	5.7	9.3	1.0	0.0	0.1	1.3	1.0	61.4	6.4	1165.2	223.4	3.9	0.4	3.3	0.3	1187.2	91.1	1.6	0.1	8.3	1.7	6.5	11.3	53.8	8.6
7.5	10	5.7	7.7	2.2	0.0	0.2	1.4	1.0	63.4	11.4	1049.4	262.0	11.5	0.6	2.8	0.6	943.7	313.2	1.8	0.3	9.4	3.6	17.7	4.5	57.0	14.0
7.5	20	5.7	10.1	3.6	0.2	0.3	4.3	0.9	102.3	14.3	1234.5	66.8	20.3	0.9	3.5	1.2	1236.1	369.8	2.0	0.7	5.6	3.1	22.5	14.7	73.9	5.9
7.5	40	5.7	7.5	0.3	0.2	0.4	2.6	0.4	83.9	5.0	1055.1	256.2	40.8	0.3	2.7	0.1	935.8	33.1	1.6	0.0	9.0	6.0	8.7	11.4	64.9	2.8
15	0	5.6	23.6	2.5	0.0	0.3	8.3	12.5	9.8	9.8	5262.2	5987.8	2.7	1.9	1.6	1.4	128.5	95.8	0.5	0.1	7.6	9.3	7.6	13.2	20.4	14.3
15	10	5.6	27.0	1.7	3.5	3.9	16.0	7.1	22.9	7.1	6366.1	1747.4	12.4	1.0	2.1	0.5	80.0	33.3	0.6	0.1	3.8	4.4	24.8	19.5	23.0	9.8
15	20	5.6	30.7	0.5	0.6	0.2	4.3	1.5	9.7	3.4	1541.1	1320.5	22.7	1.1	1.0	0.3	23.3	12.2	0.5	0.0	2.2	3.8	20.4	7.0	5.4	2.4
15	40	5.6	35.7	0.4	0.3	0.5	1.8	1.7	4.2	1.4	1181.4	52.9	47.1	1.0	1.0	0.1	15.7	1.1	0.5	0.0	0.9	1.1	21.4	7.3	4.5	0.9
Limit*				-	0.2		0.6		5								11 - F				20		7.2		40	

548 *Annual average environmental quality standards for surface waters (other than inland surface waters) (Council of the European Union, 2009) **± standard deviation

 Table 5 Kinetic experiment. Metal concentration release over time ± (standard deviation).

Minutes	Ca	\pm^*	Cu	<u>+</u>	Fe	±	K	±	Mg	±	Mn	±	Na	±	Zn	±				
	mg L ⁻¹		mg L ⁻¹		mg L ⁻¹								μg L	1						
1	8.4	0.0	8699	2761	1369	238	134.8	2.4	1.6	0.1	280.2	18.3	2.6	0.0	13045	1163				
5	8.1	0.2	12570	121	1358	168	135.8	0.8	1.3	0.0	231.8	8.1	2.2	0.0	15905	308.				
10	5.9	2.9	6570	8573	667	441	137.1	3.9	0.6	0.8	187.4	52.9	1.8	0.5	8218	10905				
15	4.2	1.9	6180	2491	732	86.0	69.3	27.2	0.6	0.2	118.8	43.4	1.2	0.6	7421	2840				
30	3.2	0.0	9014	345	817	28.6	62.5	3.2	0.5	0.0	105.7	8.6	0.8	0.0	10318	842				
60	6.1	1.4	14918	4294	973	192.0	109.2	19.5	0.9	0.2	165.6	34.1	1.5	0.3	16564	4295				
± standard	\pm standard deviation																			



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